

# Reactive Modelling of River Bank Filtration

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# Approach to reactive modelling

- Establish and calibrate a flow model
- Verification of conservative transport
  - Residence time, particle tracking analysis
- Set up a reactive transport model
  - Process analysis
  - Reaction network
  - implementation and simulation
- Aim: verify the sampled hydrochemistry

# Modeling Environment (1)

- **PMWIN**
  - Flow Model (**MODFLOW**)
  - Transport (**MT3DMS**), multi species
  - Reaction (**PHT3D**)
    - Interface to PHREEQC-2 (chemical speciation)
    - Use of all skills of PHREEQC-2
      - Precipitation/dissolution of solids
      - Speciation, redox
      - Kinetics (problem adapted formulation)
      - Ion exchange

# Modeling Environment (2)

- **PHT3D (Prommer, 2001)**
  - **Definition Reaction Framework Database**
  - **Definition components**
    - as transported species (MT3DMS),
    - or immobile Species
  - **PHREEQC-2 processing for each model element**
  - **assign results to the next transport step (MT3DMS)**

# Conceptionual chemical model (geochemical response on biodegradation)

- **Biodegradation (Kinetics) only by Organic Carbon**
- **Supply of DOC by mobilisation of matrix OC**
- **Solid electron acceptors (iron & manganese oxides /oxidhydrates)**
  - Dissolution precipitation equilibria, redox half reactions
- **Dissolved electron acceptors ( $O_2$ ,  $NO_3^-$ ,  $SO_4^{2-}$ )**
  - Redox half reactions
- **Redox capacity remains constant during kinetic step**

# Reaction Network: Components

- **dissolved components (ionar equilibrium)**
  - C(4), Ca, Mg, Na, K, NO<sub>3</sub>-N, NO<sub>2</sub>-N, N<sub>2</sub>-N, NH<sub>4</sub>-N, Fe<sup>2+</sup>, Fe<sup>3+</sup>, Mn<sup>2+</sup>, Mn<sup>3+</sup>, SO<sub>4</sub>-S, S<sup>2-</sup>-S, CH<sub>4</sub>, pH, pe
- **dissolved components (Kinetics)**
  - DOC
- **solids (equilibrium)**
  - Calcite, Ferrihydrite (Fe(OH)<sub>3</sub>), Pyrolusite (MnO<sub>2</sub>), Rhodochrosite (MnCO<sub>3</sub>), FeS<sub>ppt</sub>, Siderite (FeCO<sub>3</sub>)
- **solids (Kinetics)**
  - Particular OC

# Mathematic Model (Kinetics)

## Organic Carbon

### Particular Organic Carbon (POC) Supply of DOC

$$r_{POC} = -k_{sol} \cdot (C_{DOC} - C_{DOC,limit})$$

### Dissolved organic Carbon (DOC) MONOD Kinetics

$k_{xx}$  Decay constants, MONOD constants  $K_{xx}$ , Inhibitor constants  $K_{inh,xx}$

$$r_{degrad} = r_{O_2} + r_{NO_3} + r_{MnO_2} + r_{FeOOH} + r_{SO_4}$$

$$r_{O_2} = -k_{O_2} \cdot C_{DOC} \cdot \frac{C_{O_2}}{K_{O_2} + C_{O_2}}$$

$$r_{NO_3} = -k_{NO_3} \cdot C_{DOC} \cdot \frac{K_{inh,O_2}}{K_{inh,O_2} + C_{O_2}} \cdot \frac{C_{NO_3}}{K_{NO_3} + C_{NO_3}}$$

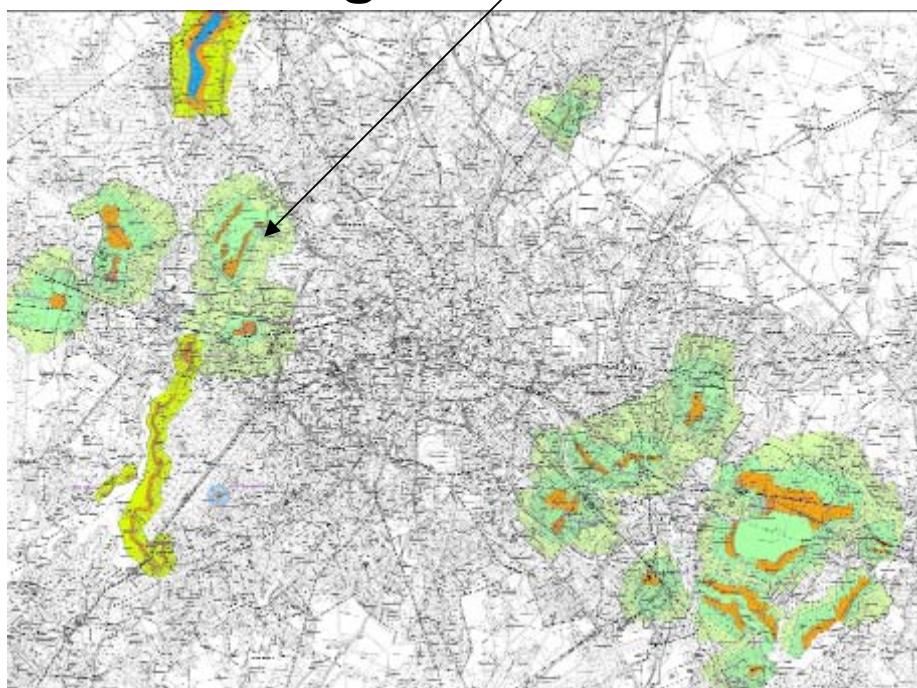
$$r_{MnO_2} = -k_{MnO_2} \cdot C_{DOC} \cdot \frac{K_{inh,O_2}}{K_{inh,O_2} + C_{O_2}} \cdot \frac{K_{inh,NO_3}}{K_{inh,NO_3} + C_{NO_3}} \cdot \frac{C_{MnO_2}}{K_{MnO_2} + C_{MnO_2}}$$

$$r_{FeOOH} = -k_{FeOOH} \cdot C_{DOC} \cdot \frac{K_{inh,O_2}}{K_{inh,O_2} + C_{O_2}} \cdot \frac{K_{inh,NO_3}}{K_{inh,NO_3} + C_{NO_3}} \cdot \frac{K_{inh,MnO_2}}{K_{inh,MnO_2} + C_{MnO_2}} \cdot \frac{C_{FeOOH}}{K_{FeOOH} + C_{FeOOH}}$$

$$r_{SO_4} = -k_{SO_4} \cdot C_{DOC} \cdot \frac{K_{inh,O_2}}{K_{inh,O_2} + C_{O_2}} \cdot \frac{K_{inh,NO_3}}{K_{inh,NO_3} + C_{NO_3}} \cdot \frac{K_{inh,MnO_2}}{K_{inh,MnO_2} + C_{MnO_2}} \cdot \frac{K_{inh,FeOOH}}{K_{inh,FeOOH} + C_{FeOOH}} \cdot \frac{C_{SO_4}}{K_{SO_4} + C_{SO_4}}$$

# Waterworks protection areas Berlin

## Tegel Waterworks

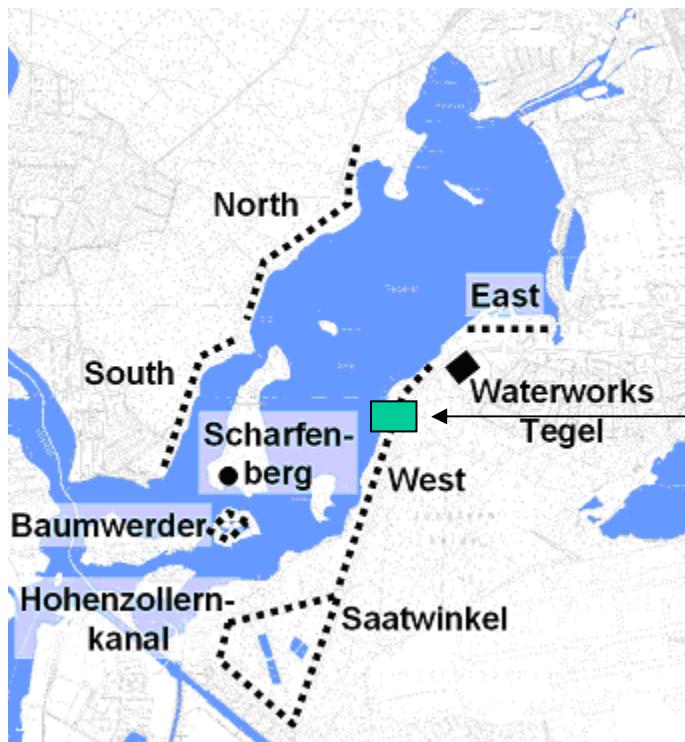


### Schutzzonen

	Zone I (Fassungsbereich mit Brunnengalerien)
	Zone II (engere Schutzzzone)
	Zone III (nach Festsetzung durch Rechtsverordnung)
	Zone III A (nach Festsetzung durch Rechtsverordnung)
	Zone III B (nach Festsetzung durch Rechtsverordnung)
	Zone III (nach 46er Anordnung)
	Schutzgebietsgrenze in Brandenburg
	Betriebsgelände Wasserwerk
	Schutzzone auf Gewässerfläche
	Blattschnitt entsprechend der Anlage zur Wasserschutzgebietsverordnung

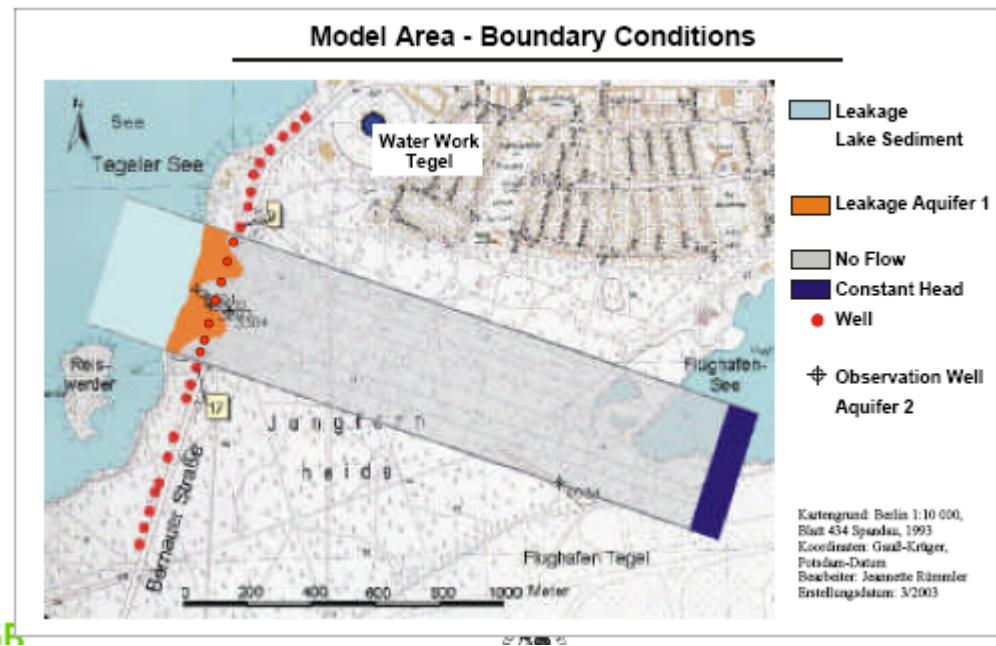
SENSUT Berlin (2006)

# Well production areas Lake Tegel



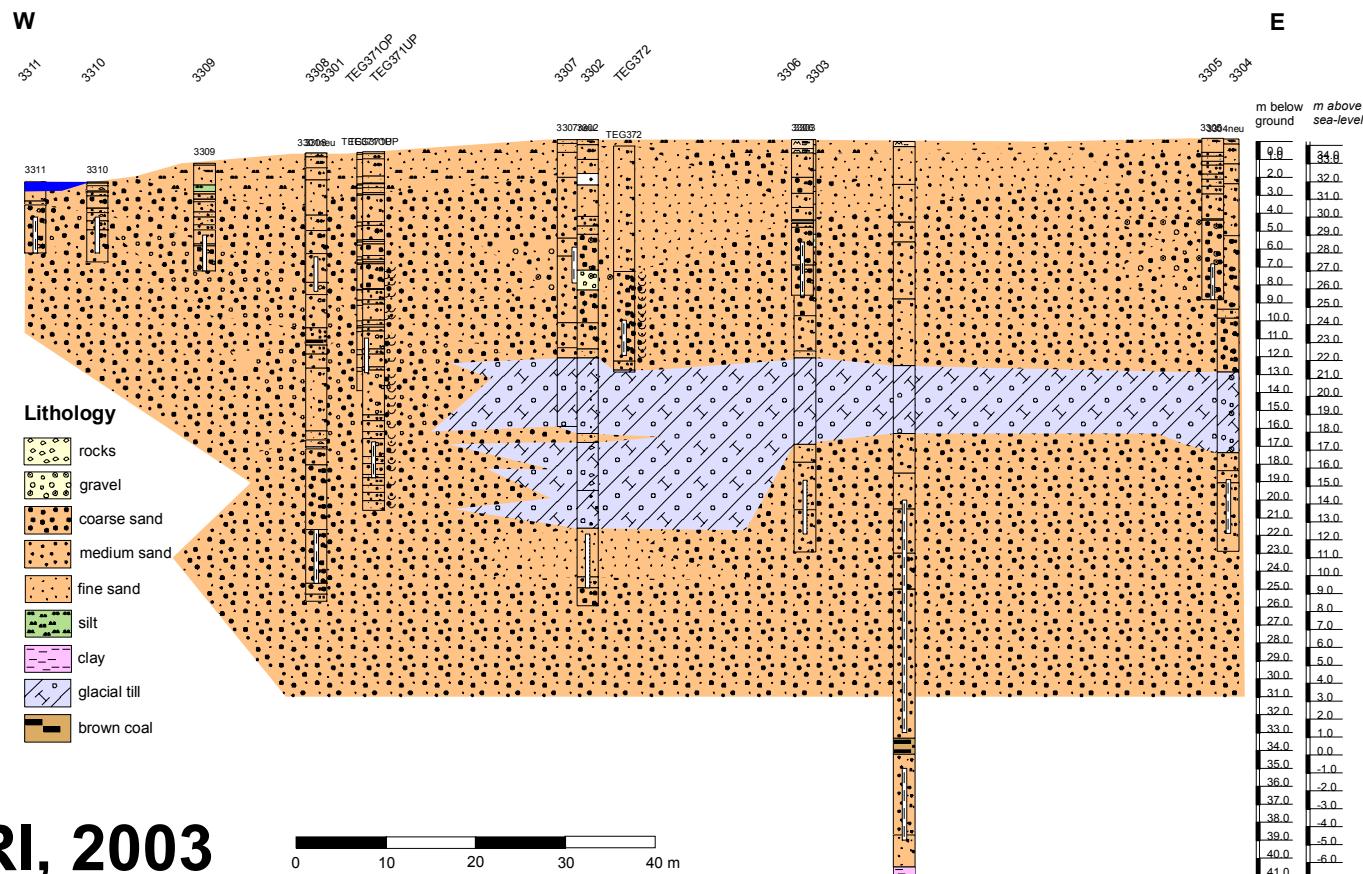
Modelling Area

# Modelling Area



Funded by NASRI (Natural and Artificial  
Systems for Recharge and Infiltration) set up  
by VEOLIA Water

# Hydrogeological section along the transect Lake Tegel

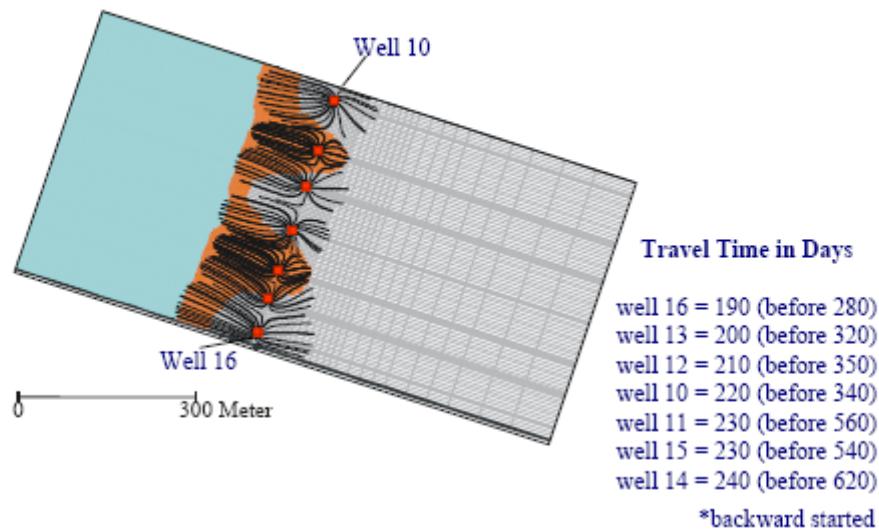


NASRI, 2003



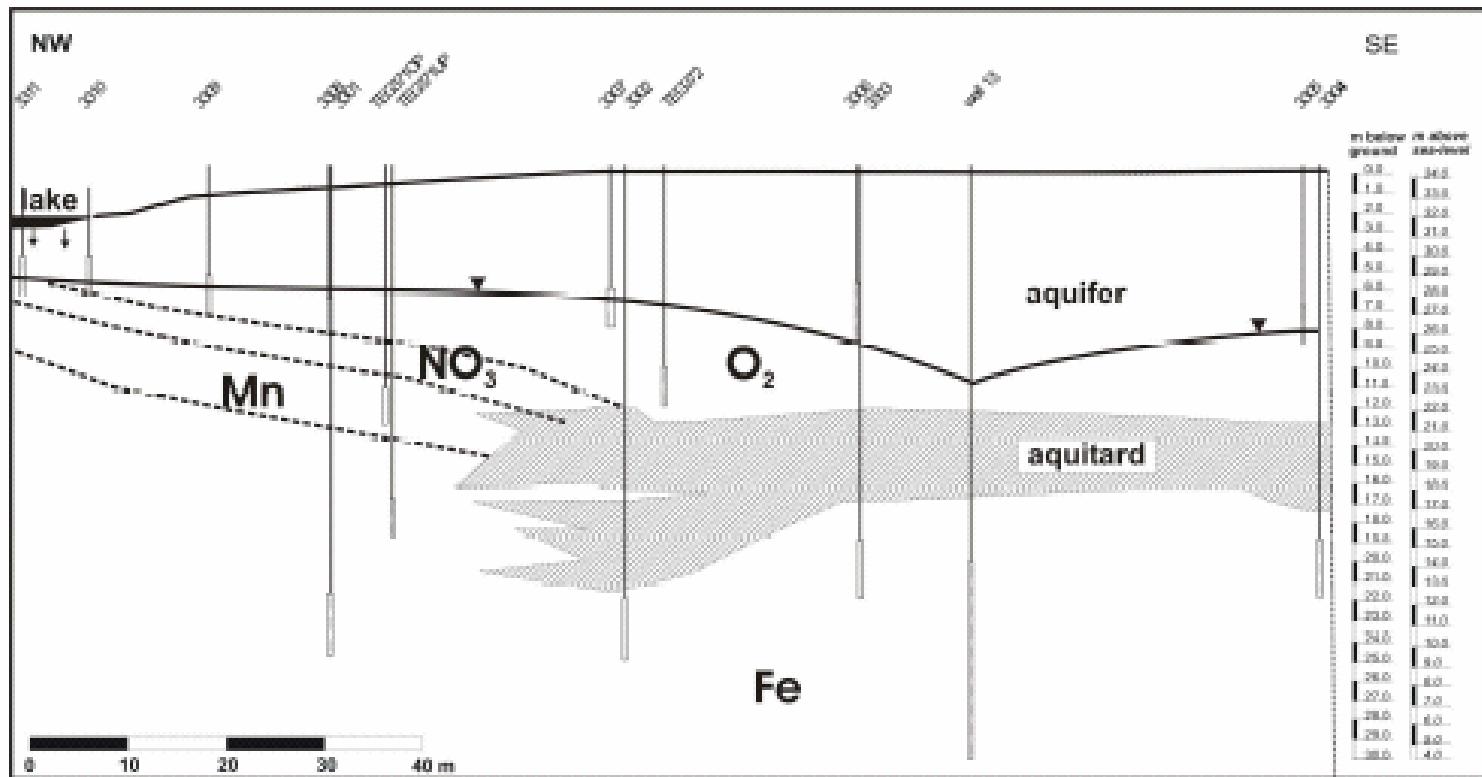
# Bank filtration flow modelling

Steady-state model – travel time towards Well\*



NASRI, 2003 (Diplomarbeit Rümler)

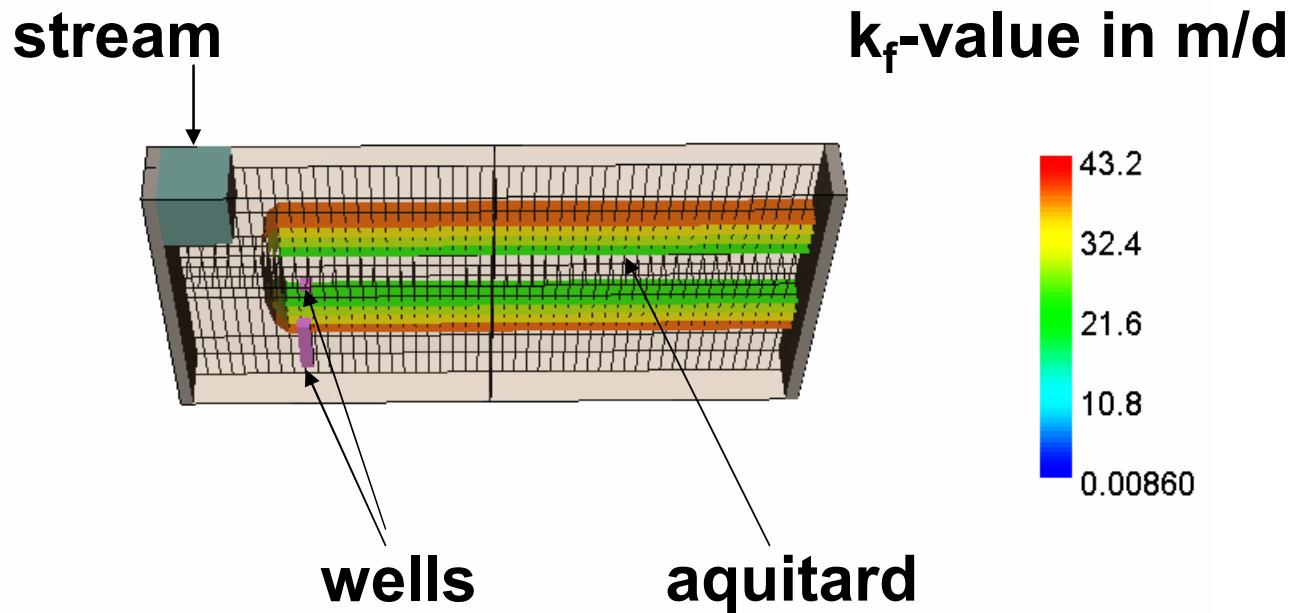
# Hydrochemistry: observed redox zonation



# Conceptual reactive Transport model

- 3D Model
  - lateral extension 1000 m x 50 m,
  - thickness of 50 m
  - Constant potential on the landside boundary
  - leakage with semipermeable colmation at the left boundary („Lake Tegel“)
  - Oscillating pumping regime
  - local geological setting conceptionally incorporated

# 3D Model configuration

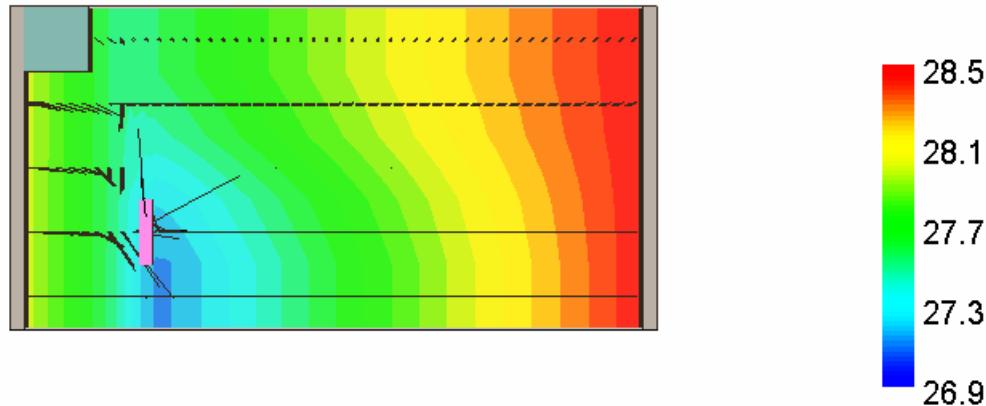


# Pumping regime

- The pumping regime at Wellfield West Tegel is strongly instastionary.
- 3 modelled alternating pumping wells
  - 2 wells Q max. 450 m<sup>3</sup>/d at the model margin
  - 1 well Q max 900 m<sup>3</sup>/d
  - Simulation: after 1 year start of pumping, total simulation duration 3 years
  - Alternating pumping 10 days interval
  - If the central well is pumping the other wells are switched off (and the reverse)

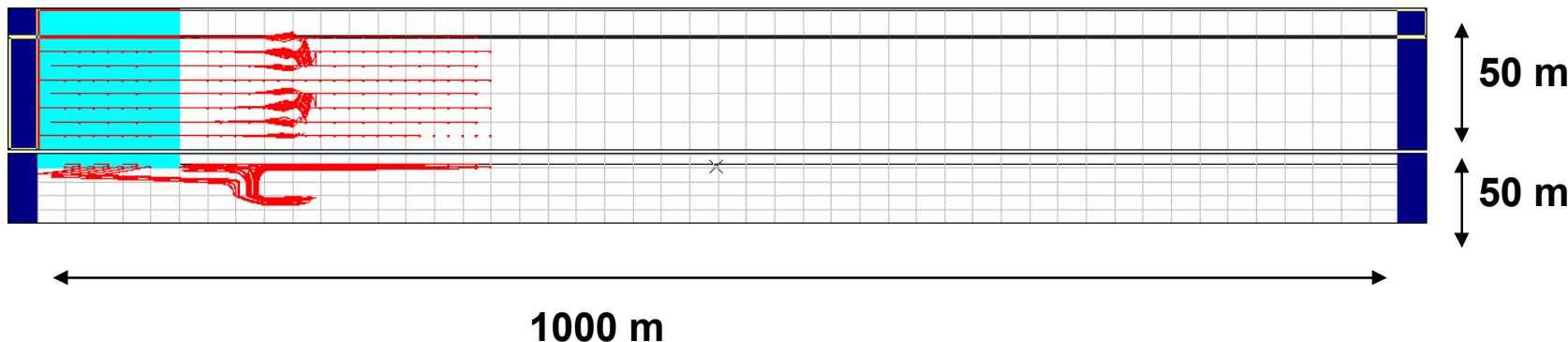
# Simulated piezometer heads during pumping

**Piezometer head (m a. s. l.)**



# Flow pathes during oscillating pumping

**Plan view**



**Vertical view**

**instationary flow field, variable pumping**

# Assigning initial and boundary reactive transport conditions

- **Initials**
  - Based on groundwater analyses
  - Problem: matrix composition
- **Boundary conditions**
  - Based on surface water analyses (Lake Tegel)
  - Inflow land side: groundwater analyses

# Presentation of reactive transport calculation results

- prognostic simulation of hydrochemistry instationary pumping conditions
- Simulation time 3 a
- Chemical initials and boundary conditions from NASRI data base

# Chemical initials and boundary conditions (1)

Component	Initials+constant head cells Oxic	Initials+constant head cells Anoxic	Inflow concentration stream
pH	6.918	7.212	8.20
pe	13.791	1.458	4.34
C(+4)	5.668e-003	3.296e-003	2.837e-3
C(-4)	1e-20	1e-20	1e-20
Ca	4.174e-003	2.938e-003	2.239e-3
Na	1.302e-003	1.428e-003	2.185e-3
Mg	7.741e-004	3.169e-004	4.568e-4
Cl	1.242e-003	1.609e-003	1.97e-3
K	5.146e-005	4.018e-005	3.019e-4
N(+5)	1.258e-004	1e-20	1.429e-4
N(+3)	1.786e-017	1e-20	1.08e-16
N(0)	1e-20	1.572e-005	3.696e-23
N(-3)	1e-20	1e-20	1e-20

# Chemical initials and boundary conditions (2)

Component	Initials+constant head cells Oxic	Initials+constant head cells Anoxic	Inflow concentration stream
Fe(2)	3.020e-017	1.320e-005	1e-20
Fe(3)	4.437e-008	3.311e-008	1e-20
Mn(2)	9.895e-015	7.882e-006	1e-20
Mn(3)	1e-20	1e-20	1e-20
S(-2)	1e-20	1e-20	1e-20
S(6)	2.636e-003	1.729e-003	1.448e-3
O(0)	1.134e-003	1e-20	1.113e-3
DOC	1e-7	1e-4	1e-5
POC	1e-4	0.02	0.00
Calcite	0.014775	0.01479	0.00
Ferrihydrite Fe(OH) <sub>3</sub>	0.0283	0.0283	0.00
Pyrolusite MnO <sub>2</sub>	0.00095	0	0.00
Rhodochrosite MnCO <sub>3</sub>	0	0.00095	0.00
Siderite FeCO <sub>3</sub>	0	8.32e-6	0.00

# Chemical boundary conditions recharge (1)

Komponente	Recharge (GWN)
pH	4.056
pe	16.566
C(+4)	1.082e-5
C(-4)	0.00
Ca	2.233e-5
Na	6.189e-5
Mg	2.334e-5
Cl	8.295e-5
K	6.366e-5
N(+5)	1.934e-4
N(+3)	4.089e-17
N(0)	0.00
N(-3)	0.00

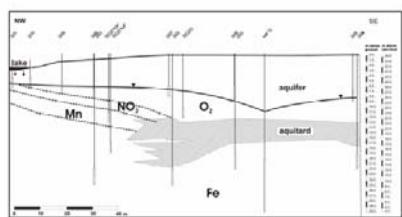
Groundwater recharge:  
100 mm/a

# Chemical boundary conditions recharge (2)

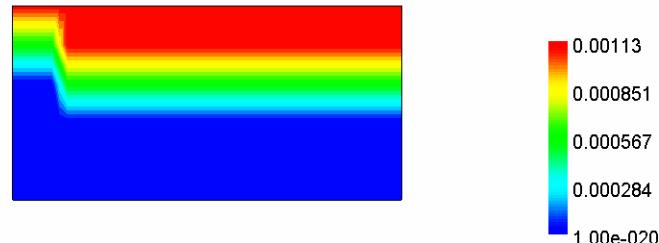
Component	Groundwater Recharge
Fe(2)	1e-20
Fe(3)	1e-20
Mn(2)	1e-20
Mn(3)	1e-20
S(-2)	0.00
S(6)	5.462e-5
O(0)	5.012e-4
DOC	0.00
POC	0.00
Calcite	0.00
Ferrihydrite Fe(OH) <sub>3</sub>	0.00
Pyrolusite MnO <sub>2</sub>	0.00
Rhodochrosite MnCO <sub>3</sub>	0.00
Siderite MnCO <sub>3</sub>	0.00

# Results (1):O<sub>2</sub>

Observation

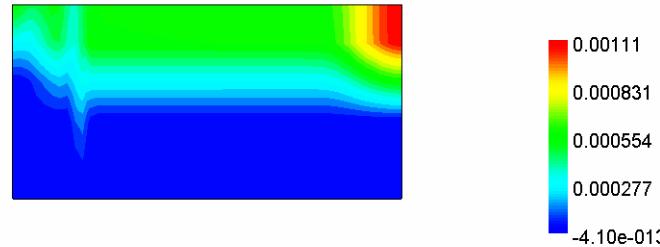


Simulation

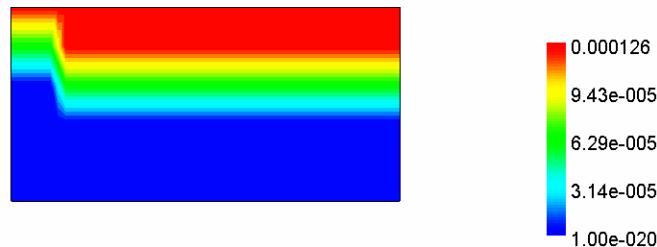
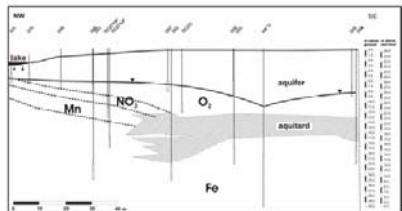


Start

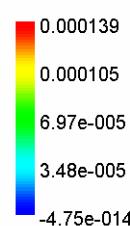
after 3 a



# Results (2):NO<sub>3</sub>-N



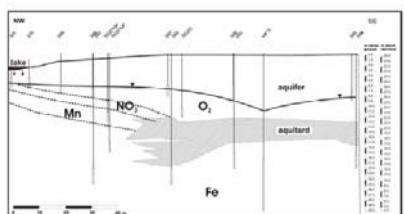
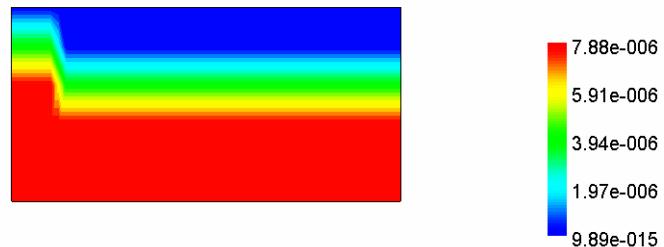
Start



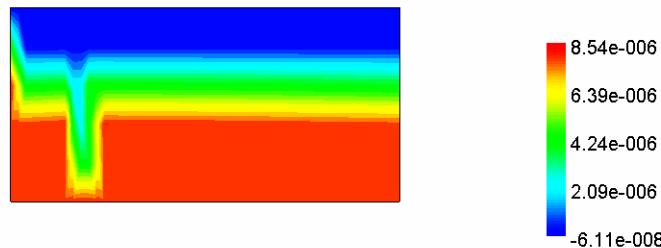
nach 3 a

# Results (4):Mn

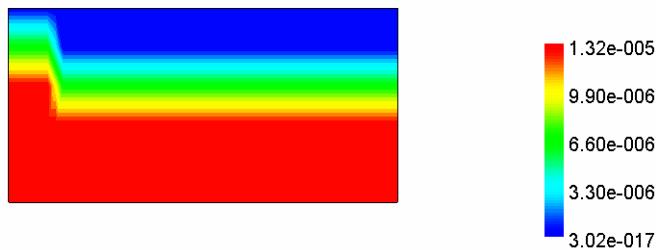
Start



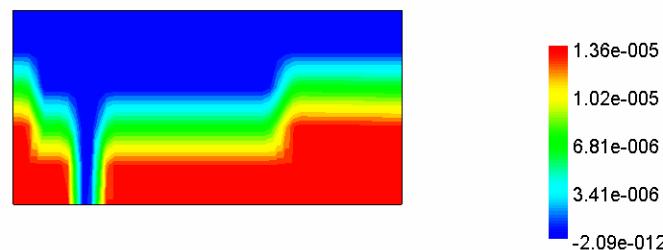
nach 3 a



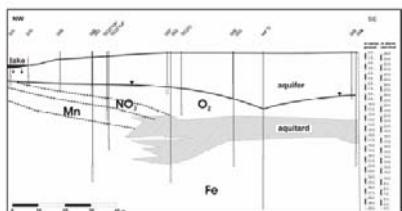
# Results (5): Fe



**Start**



**after 3 years**



# Conclusions

- **Reactive transport modelling is a useful tool**
  - For all problems and test sites involving changes in hydrochemical groundwater compositions
  - To define redox conditions for the stability /instability of pharmaceutical trace compounds during river bank filtration

**Thank you very much for  
your attention!**